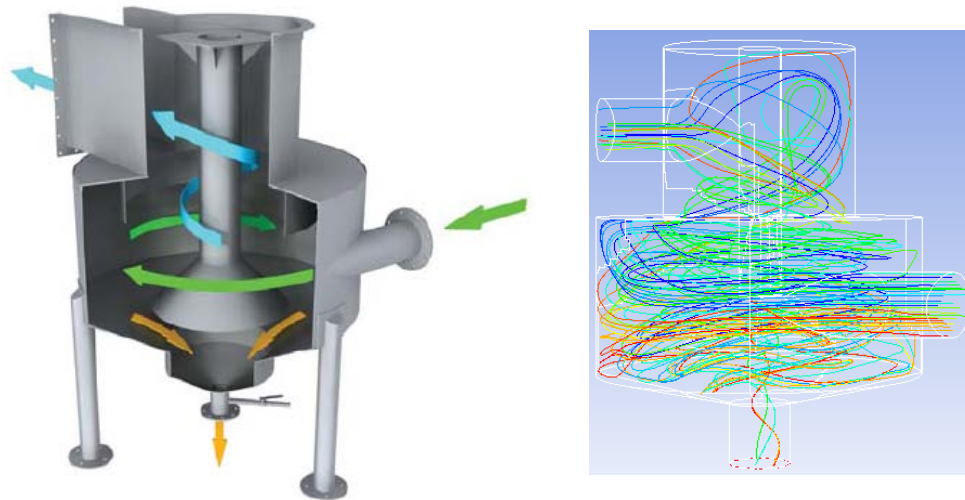


# Computational Analysis on Multiphase Flow in a Vortex Separator as Intake Device for Sea Water

Sungsu Lee, Hyun Ah Son, Chungbuk National University, Korea

Albert S. Kim, University of Hawaii at Manoa, USA

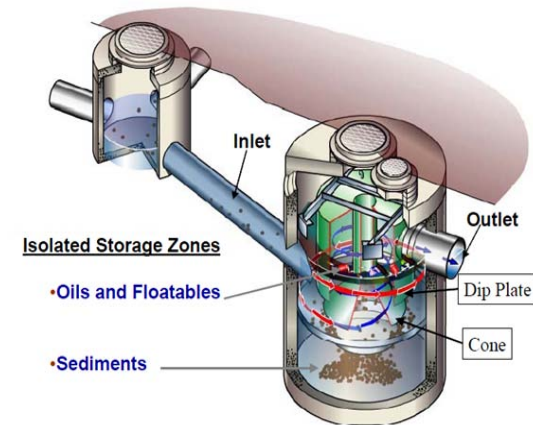
Hyun Ju Kim, KIOST, Korea



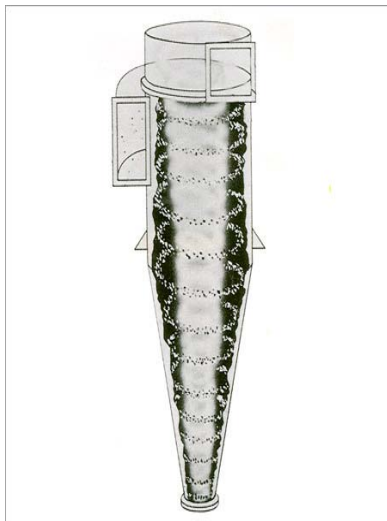
# I. INTRODUCTION

## Vortex Separator

Deep sea water intake system is under development, and vortex separator for separating particulate matter from the seawater is recommended.



Downstream Defender® HDVS



Bhaskar, Mineral Eng (2007)

- Flow forced into tangential inlet under pressure causing flow to spin
- Pressure gradients within cyclone create two vortices, one inside the other, spinning in same direction but with opposite axial direction
- Density difference between water and solids causes water collect at axial core
- Dense phase exits at “underflow” & light phase exits at “overflow” adjacent to inlet

# II. COMPUTATIONAL MODEL

- **Materials**

Water Density : 998.2 kg/m<sup>3</sup>

Particulate Density : 2300kg/m<sup>3</sup>

Mass fraction of solid phase at inlet : 10%  
particle diameter : 10, 20, 30, 40μm

- **Boundary conditions**

inlet : mass flow rate 1.3kg/s

wall : no-slip

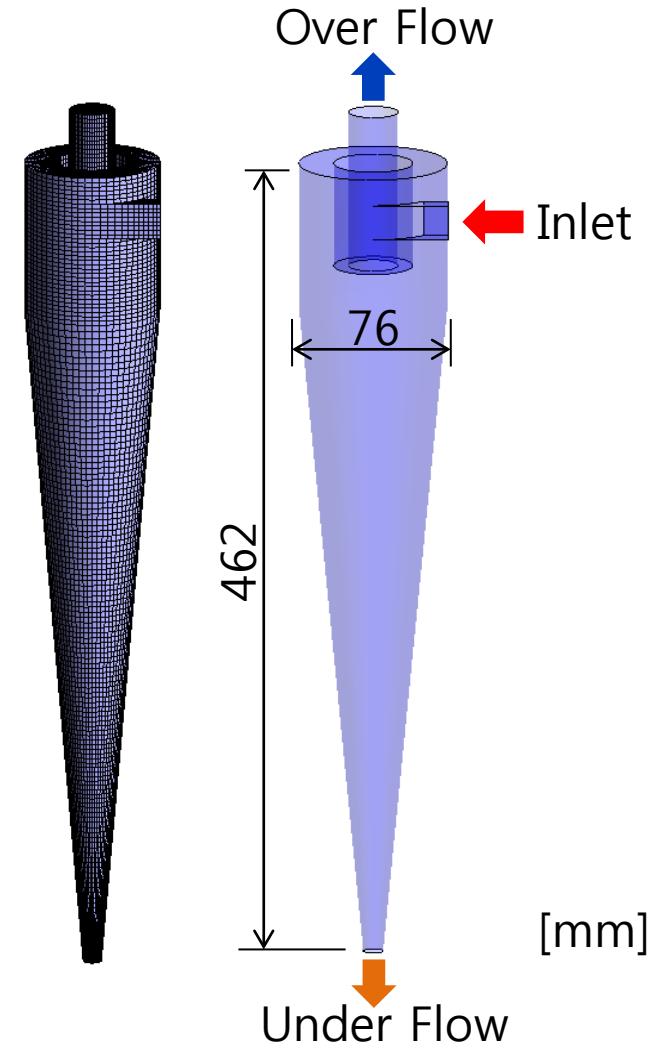
- **Two-Phase (Liquid-Solid), Granular Flow**

Re = 31000 (Inlet Velocity, Diameter)

Euler-Euler Model

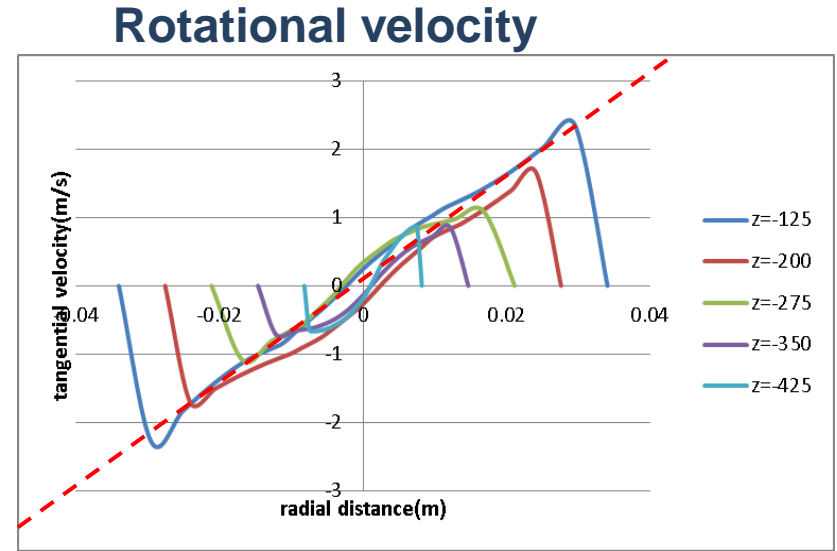
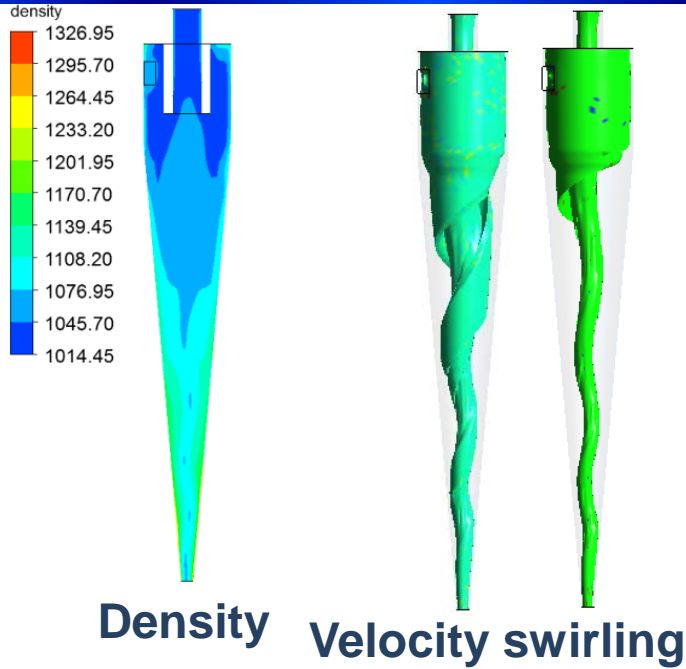
$$\frac{\partial}{\partial t} (a_k \rho_k) + \nabla \cdot (a_k \rho_k \vec{v}_k) = 0$$

$$\frac{\partial}{\partial t} (a_k \rho_k \vec{v}_k) + \nabla \cdot (a_k \rho_k \vec{v}_k \vec{v}_k) = -a_k \nabla p + \nabla \cdot \bar{\tau}_k + \sum_{p=1}^n \vec{R}_{qk} + a_k \rho_k \vec{g} + (\vec{F}_k + \vec{F}_{lift,k} + \vec{F}_{vm,k})$$

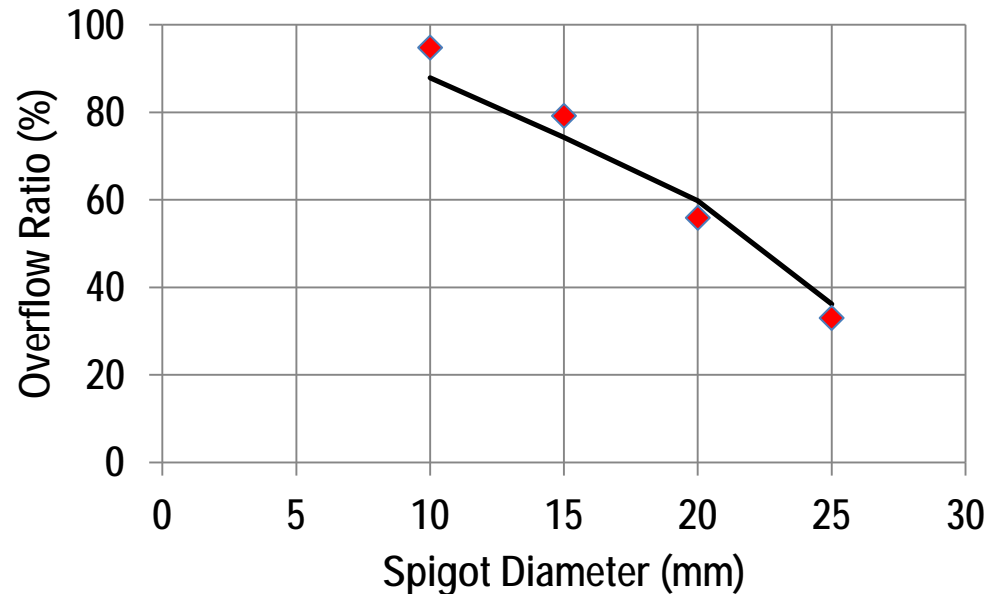


Bhaskar, Mineral Eng (2007)

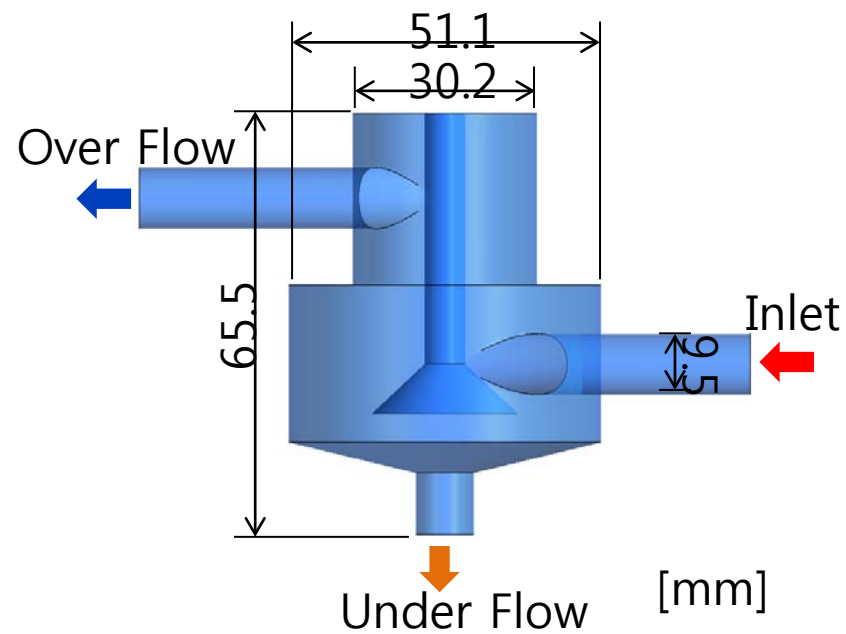
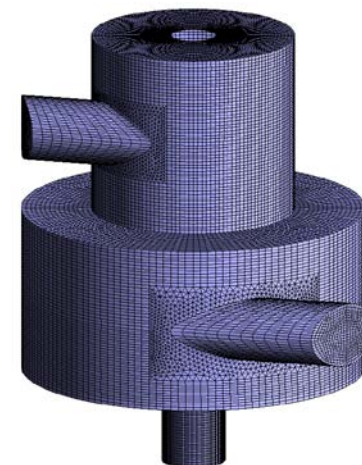
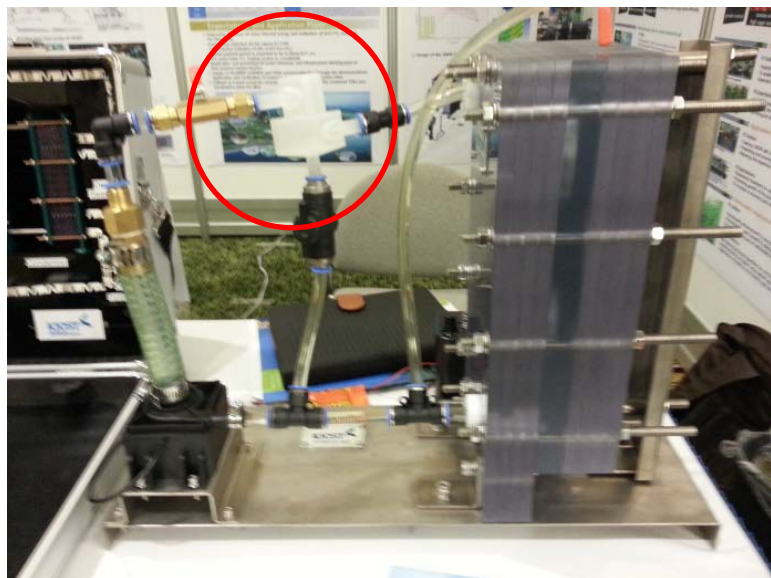
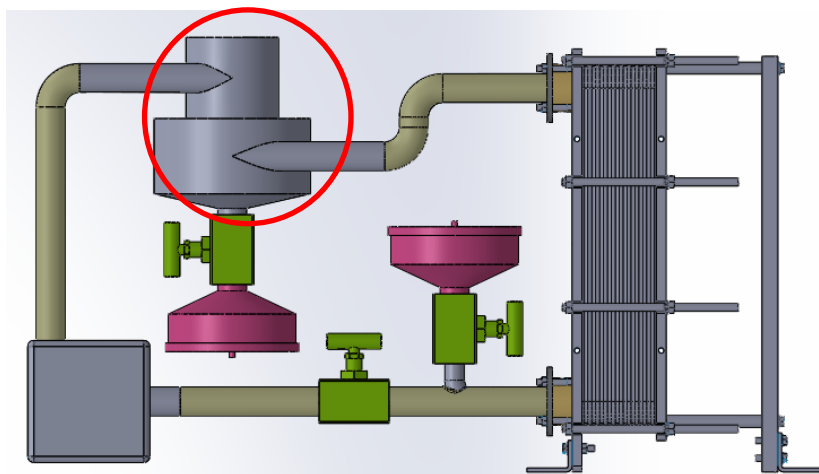
# III. VALIDATION



◆ Exp (Bhaskar, 2007) — Present



# IV. VORTEX SEPARATOR



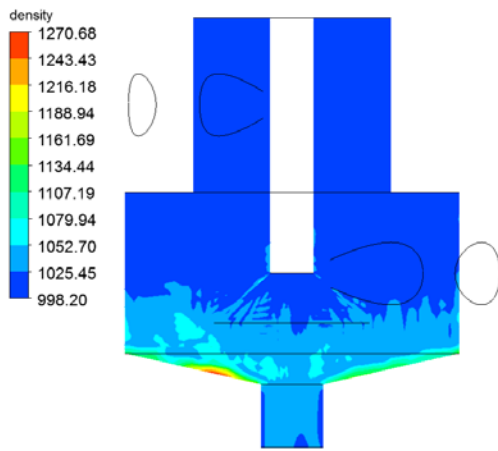
# IV. VORTEX SEPARATOR

## Materials

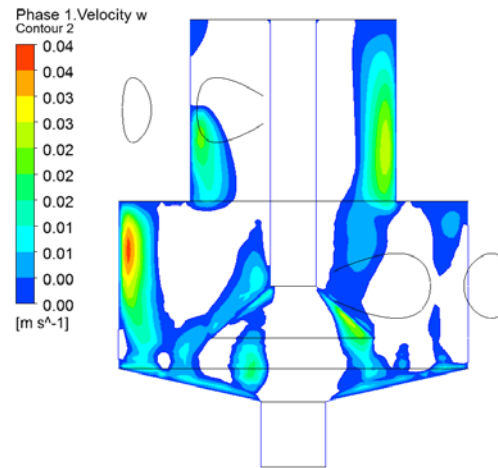
- Water Density : 998.2 kg/m<sup>3</sup>
- Particle Density : 2645kg/m<sup>3</sup>
- Particle Diameter : 2mm
- Particle Mass Fraction : 22% (Inlet)

## Boundary conditions

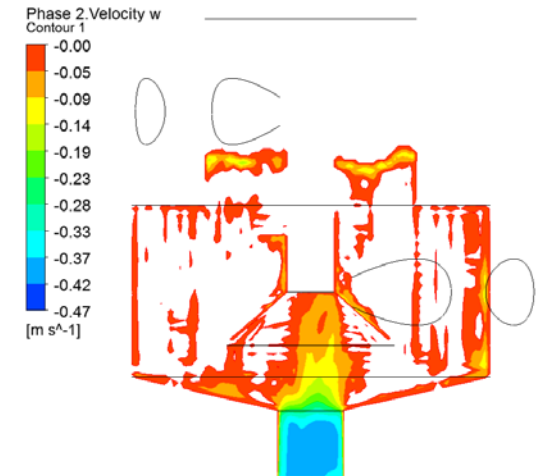
- mass flow rate 0.01~0.1kg/s
- Two-Phase (Liquid-Solid), Granular Flow**  
Re = 1250~12500



Density



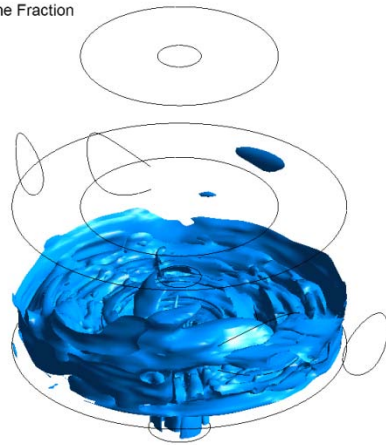
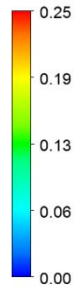
Water axial velocity



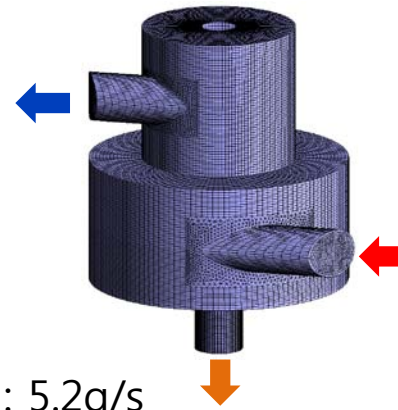
Solid axial velocity

# V. COMPUTATIONAL RESULTS

Phase 2. Volume Fraction  
vt02



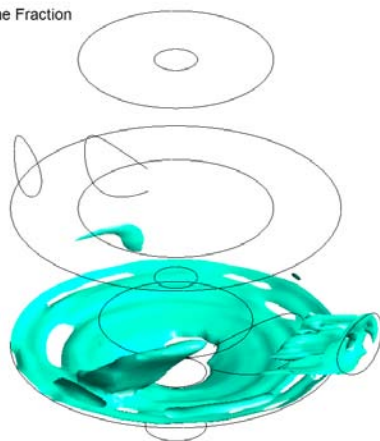
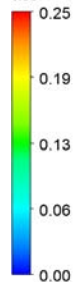
MFR : 4.8g/s  
SLF : 62%  
SPF : 0%



MFR : 10g/s  
PMF : 22%

MFR : 5.2g/s  
SLF : 38%  
**SPF : 100%**

Phase 2. Volume Fraction  
vt05



MFR : Mass Flow Rate  
SLF : Separated Liquid Fraction  
SPF : Separated Particle Fraction

- Complete Filtering is Achieved
- Need to Increase SLF(Over Flow)

Solid iso-volume fraction(3%,8%)

# VI. CONCLUDING REMARKS

- Present numerical scheme well simulates flow field inside vortex separator
- Flow inside reflects forced vortex field with linearly decreasing magnitude rotational velocity before it reaches dividing depth.
- When particle diameter reaches up to 2mm, the solid phase is completely separated from liquid phase, showing effective filtering process.
- Will be scaled to prototype based on computational & experimental model



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